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## VOLUMETRIC AND PHASE BEHAVIOR OF MIXTURES OF NITRIC CMIDE AND NITROGEN EXCHIDE

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## ABSTRACT

The oxides of nitrogen are potentially useful as exidents in special fuel systems. Mixtures of nitric oxide and nitrogen dioxide are particularly promising because of the lower freezing point which results from the addition of small quantities of nitric oxide to nitrogen dioxide.

A knowledge of the volumetric and phase behavior of mixtures of nitric oxide and nitrogen dioxide is of utility in the design of equipment for the storage and delivery of these compounds to combustion equipment.

The compositions of the coexisting phases of mixtures of nitric oxide and nitrogen dioxide were established throughout the two-phase region for temperatures above 70° F. and for compositions containing more than 0.80 weight fraction of nitrogen dioxide. The specific volumes of the liquid and gas phases of mixtures of these oxides were determined at temperatures between 40° F. and 340° F. for pressures up to 7,000 pounds per square inch. The results are presented in tabular and graphical form.

The bubble point pressure of mixtures of these oxides of nitrogen containing as much as 0.2 weight fraction of nitric oxide is below 300 pounds per square inch at 160° F. Such pressures are low enough to permit the use of conventional means of storage and handling of the

mixtures of the oxides of nitrogen under most climatic conditions.

The specific volume changes almost linearly with isobaric-isothermal change in composition in both the liquid and the gas phases, thus permitting ready interpolation of the results to any desired composition within the range of investigation. The data obtained are consistent with measurements already available for the volumetric and phase behavior of the pure components.

(The abstract is intended for publication in a separate section of the journal).

VOLUMETRIC AND PHASE BEHAVIOR OF MIXTURES OF NITRIC OXIDE AND NITROGEN DIOXIDE

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## INTRODUCTION

The phase behavior of mixtures of mixic oxide and mitrogen dioxide has not been studied at elevated pressures. Epstein and Cirkova (3) determined the two-phase pressures of mixtures of these oxides of nitrogen containing as much as 0,35 weight fraction of mitric oxide at temperatures between 68° F. and 140° F. for pressures below 240 pounds per square inch. The compositions of the mixtures investigated were related to the earlier measurements of Baume and Robert (1), who studied this binary system at temperatures below 68° F. Wittorf (19) determined the limits of solubility of mitric oxide in mitrogen dioxide in the same range of temperature as was reported by Saume and Robert. Purcell and Cheesman (9) measured the solubility of nitric oxide in mitrogen dioxide at temperatures below 510 F. for pressures less than 68 pounds per square inch. Whittaker and coworkers (17) determined the two-phase pressure for six mixtures of nitric oxide and nitrogen dioxide for compositions containing up to 0, 169 weight fraction of nitric oxide. The measurements were made at temperatures between -400 and 59° F. Their results are in reasonable agreement with those of Baume and Robert (1).

The effect of pressure and temperature upon the specific volume of

the components has been investigated in some detail. Briner and co-workers (2) established the volumetric behavior of nitric oxide at low temperatures and Johnston and Weimer (6) determined the second virial coefficient at temperatures up to 70° F. for pressures below one atmosphere. Recently the volumetric behavior of this compound was studied at pressures up to 2,500 pounds per square inch for temperatures between 40° and 220° F. (4).

Verhoek and Daniels (16) and Mittasch and coworkers (3) determined the volumetric behavior of nitrogen dioxide in the gaseous region for temperatures below 113° F. Scheffer and Treub (12) measured the vapor pressure of this compound up to the critical temperature. Recently additional measurements have extended the knowledge of the volumetric behavior of the liquid and gas phases of this compound to temperatures of 340° F, and pressures up to 7,000 pounds per square inch (10,13). Kobe and Pennington (7) recently reviewed the thermochemical characteristics of nitrogen and its oxides.

The present measurements are concerned with the volumetric behavior of 15 mixtures of nitric oxide and nitrogen dioxide at compositions containing as much as 0,2 weight fraction nitric oxide at pressures up to 7,000 pounds per square inch in the temperature interval between 40° and 340° F. Four of these mixtures were investigated in detail and the remainder were studied throughout the indicated temperature interval at nearly a single specific volume. The dew point and bubble point states for four mixtures were determined as a function of temperature.

### METHODS

The methods employed in this investigation were similar to those described earlier for the study of the volumetric behavior of nitrogen dioxide (10,13). In principle, they involved the containment of the mixture in a spherical pressure vessel (10). The pressure within this vessel was determined by means of a pressure balance (11) which was connected to the vessel through a liquid-filled tube terminating at the sphere with a stainless steel diaphragm (10, 13). This balance was calibrated against the vapor pressure of carbon dioxide at the ice point. The pressures were established within 0.2 pound per square inch or 0.1%, whichever measure yielded the larger uncertainty.

The pressure vessel was immersed in an agitated temperature-controlled bath of a silicone and the temperature was measured by means of a platinum resistance thermometer which had been compared recently with a similar instrument calibrated by the National Bureau of Standards. These comparisons were made with such care and the temperature of the bath was so steady that the temperature within the working vessel was known relative to the international platinum scale with a probable error of 0.03° F.

The weight of each of the components was determined gravimetrically by the use of weighing bomb techniques (11). The total quantity of sample originally introduced was established with a probable error of not more than 0.03% and the compositions of the mixtures were known with a standard error of 0.0012 mole fraction. After each set of measurements of a sequence of corresponding pressures and temperatures, a portion of the sample was withdrawn at a state in the single-phase region

and another sequence of pressures and temperatures was then determined. A total of from five to ten series of such measurements were made with each of the four mixtures. In the end the entire sample was withdrawn and the cumulative weights of the mixture removed were compared with the original weight. In each case it was found that the weight of the oxides of ritrogen withdrawn agreed within 0.1% with that added. Such agreement was one more indication of the relatively small uncertainty in the weights of the material involved in the several sets of measurements.

Phase boundaries for the mixtures were established from discontinuities of the pressure-temperature derivatives which occurred at these points. The specific volume of the mistures at each of the states investigated was determined from the weight of the material within the pres sure vessel and the total volume of the container. The latter value was established from calibrations with a known weight of liquid water at relatively low pressures for a series of temperatures. The studies of Smith and Keyes (15) were employed to determine the specific volume of water as a function of pressure and temperature. The changes in volume of the container with pressure and temperature were ascertained from the thermal expansion and Young's modulus of the steel. The spherical shape and nearly uniform wall thickness permitted the changes in volume to be established with accuracy. Excellent agreement was obtained between the variation in volume of the pressure vessel with temperature established from the calibration with water and that predicted from the thermal expansion of the steel. Deviations of 2s much

pressures above 7,000 pounds per square inch were found between the values established from the volumetric behavior of water (15) and those predicted from Young's modulus of the steel and the volume of the vessel at low pressures. In the present study the specific volumes of the mixtures were based upon the total volume of the pressure vessel at 70° F. and atmospheric pressure and the properties of the steel. It is believed that the specific volumes were known with a standard error of 0.18% throughout the ranges of pressure and temperature investigated.

## MATERIALS.

The nitric oxide utilized in this work was obtained from The Matheson Co. and was purified by the method described by Johnston and Giauque (5), involving absorption of impurities and subsequent fractionation and sublimation. The specific weight of a sample of the purified gas at atmospheric pressure indicated that it probably contained less than 0.002 weight fraction of material other than mitric oxide. The nitrogen dioxide, obtained from the Allied Chemical and Dye Corp., was purified by fractionation at atmospheric pressure in a glass column containing 16 plates. The fractionation was carried out at a reflux ratio of 10 and the middle 60% of the overhead was retained for final purification. This partially purified material was passed over phosphorous pentoxide at a pressure of one atmosphere and condensed at the temperature of liquid mitrogen at a pressure below 0.001 inch of mercury. The vapor pressure of the purified nitrogen dioxide was in good agree-

ment with earlier values (13). It is believed that it contained less than 0.003 weight fraction of material other than nitrogen dioxide. The purified samples of the oxides of nitrogen were stored at pressures higher than atmospheric in stainless steel containers until used.

## EXPERIMENTAL RESULTS

Typical sets of pressure-temperature measurements for mixtures containing 0.8312 and 0.8205 weight fractions of nitrogen dioxide are shown in Figures 1 and 2 respectively. Figure 1 presents data for the gaseous region, whereas those in Figure 2 relate to the liquid region. The data in the heterogeneous region have been omitted in the interest of clarity. The pressure-temperature diagram of Figure 3 portrays on a somewhat larger scale the behavior, near the boundaries of the heterogeneous region, of a mixture containing 0.9431 weight fraction of nitrogen dioxide. The precision of the data shown is typical of that obtained in this study. A sems of four such sets of measurements together with measurements for a single pressure-temperature sequence with each of 11 mixtures formed the experimental basis for the present results. A detailed record of the experimental determinations is available (14). A sample of this information constitutes Table I in which the pressure, temperature, and specific volume have been recorded for each of the states investigated. Because of the small change in total volume of the bomb with varying conditions, a corresponding change in the specific volume of the sample recurs. In Figures 1, 2, and 3 the

average specific volume for each of the pressure-temperature sequences has been depicted.

Figure 4 presents the compressibility factor as a function of pressure for a mixture containing 0.8312 weight fraction of nitrogen dioxide.

The values of the compressibility factor were computed in the following way:

$$Z = \frac{PVM^*}{RT} = \frac{PV}{bT}$$
 (1)

The constants in Equation 1 were based upon an atomic weight of nitrogen of 14,008 and an atomic weight of oxygen of 16,000 which correspond to the values recommended in a tabulation of atomic weights (18). A value of the universal gas constant of 10,73185 (ib. per sq. in.) (cu. ft. per ib. mole) per OR. was employed. Table II records the values of the specific volume and compressibility factor for five evenly spaced compositions within the range of the conditions which were covered in the investigation, using even values of pressure and temperature. The effect of composition upon the specific volume of this system in the liquid phase at a temperature of 160° F. is shown in Figure 5. Figure 6 presents a compressibility factor-composition diagram for a temperature of 280° F., including data at low pressures.

Figure 7 is a pressure-composition diagram for the bubble point liquid and dew point gas for the lower temperatures. The curves have been extended only over the range of compositions for which experimental measurements were obtained. The compositions of the gas phase coexisting

with liquid reported by Purcell and Cheesman (9) were interpolated to 40° F. and were taken into account in the preparation of this diagram.

Figure 8 depicts the pressure-composition relations for the higher temperatures. The behavior is much simpler for temperatures above  $100^{\circ}$  F, and the data may be interpolated with but small uncertainty. Table III records the properties of the coexisting liquid and gas phases as a function of pressure and temperature. The information recorded in this tabulation was obtained by graphical interpolation of the volumetric measurements available.

## ACKNOWLEDG& ENT

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Lacey reviewed the manuscript.

### REFERENCES

- 1. Baume, G., and Robert, N., Compt. rend., 169, 967 (1919).
- Briner, E., Biedermann, H., and Rothen, A., Helv. Chim. Acta, 8, 923 (1925); J. Chim. Phys., 23, 157 (1926).
- 3. Epstein, D. A., and Cirkova, L. A., J. App. Chem., (Russia) 12, 14 (1939).
- 4. Golding, B. H., and Sage, B. H., IND, ENG. CHEM., 43, 160 (1951).
- 5. Johnston, H. L., and Giauque, W. F., J. Am. Chem. Soc., 51, 3194 (1929).
- 6. Johnston, H. L., and Weimer, H. R., Ibid., 56, 625 (1934).
- 7. Kobe, K. A., and Pennington, P. E., Pet. Befiner, 29, 129 (1950).
- 8. Mittasch, A., Kuss, E., and Schlueter, H., Z. anorg. u. allgem. Chem., 159, 1 (1926).
- 9. Purcell, R. H., and Cheesman, G. H., J. Chem. Soc. (London), 826 (1932).
- 10. Reamer, H. H., and Sage, B. H., IND, ENG. CHEM., 44, 185 (1952).
- 11. Sage, B. H., and Lacey, W. N., Trans. Am. Inst. Mining Met. Engrs., 136, 136 (1940).
- 12. Scheffer, F. E. C., and Treuh, J. P., Z. physik. Chem., 81, 308 (1913).
- Schlinger, W. G., and Sage, B. H., IND, ENG. CHEW., 42, 2158 (1950).
- 14. Selleck, F. T., Reamer, H. H., and Sage, B. H., Washington, D. (., Am. Doc. Inst., Doc. No. (1952).
- 15. Smith, L. B., and Keyes, F. G., Proc. Am. Acad. Arts and Sci., 69, 285 (1934).
- 16. Verhoek, F. H., and Daniels, F., J. Am. Chem. Soc., 53, 1250 (1931).
- Whittaker, A. G., Sprague, R. W., Skolnik. S., and Smith,
   G. B. L., Ibid., 74, 4794 (1952).

## REFERENCES (cont.)

- 18. Wickers, E., Ibid., 72, 1431 (1951).
- 19. Wittorf, N. V., Z. anorg. Chem., 41, 85 (1904).

## NOMENGLATURE

- b specific gas constant
- M\* average molecular weight
- P pressure, 1b./sq. inch absolute
- R universal gas constant
- T absolute temperature, OR
- V specific volume, cu. ft./1b.
- Z compressibility factor

## FIGURES

- 1. Pressure-Temperature Diagram for a Mixture Containing 0,8312 Weight Fraction Nitrogen Dioxide.
- 2. Pressure-Temperature Diagram for a Mixture Containing 0, 8205 Weight Fraction Nitrogen Dioxide.
- 3. Behavior of a Mixture Containing 0.9431 Weight Fraction Nitrogen Dioxide in the Heterogeneous Region.
- 4. Compressibility Factor for a Mixture Containing 0.8312 Weight Fraction Nitrogen Dioxide.
- 5. Specific Volume-Composition Diagram for a Temperature of 160° F.
- 6. Effect of Composition upon Compressibility Factor at 280° F.
- 7. Pressure-Composition Diagram for the Lower Temperatures.
- 8. Pressure-Composition Diagram for the Higher Temperatures.

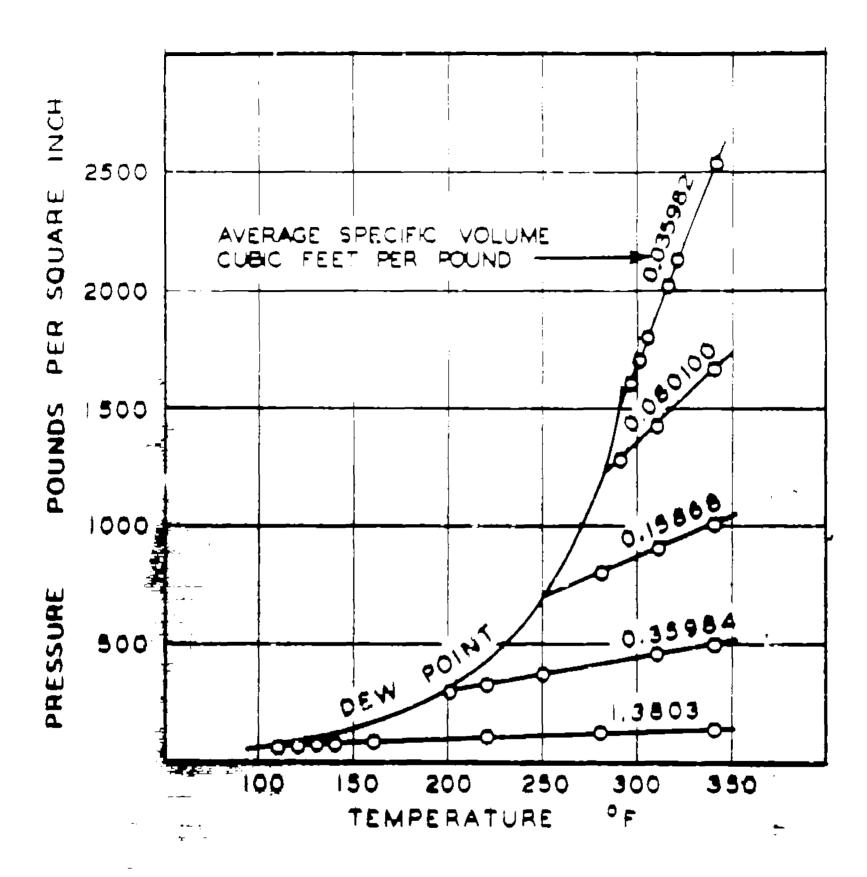
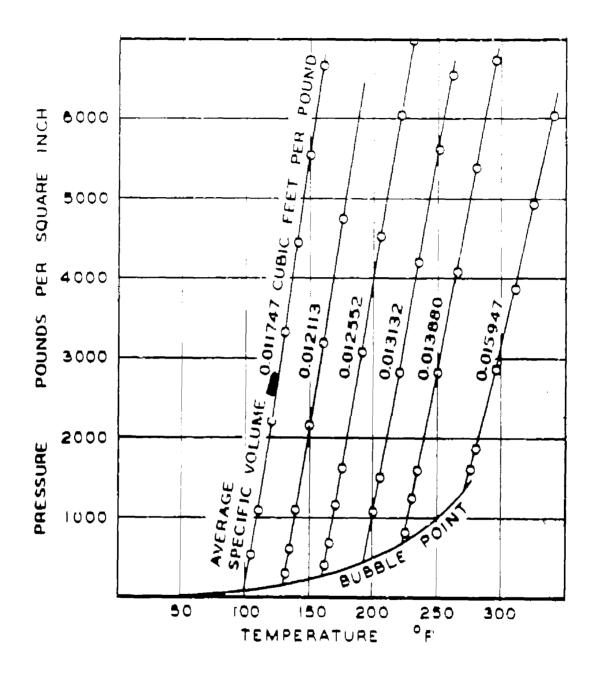


Fig. 1 Pressure-Temperature Diagram for a Mixture Containing 0, 8312 Weight Fraction Nitrogen Dioxide.



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Fig. 2 Pressure-Temperature Diagram for a Mixture Containing 0, 8205 Weight Fraction Nitrogen Dioxide.

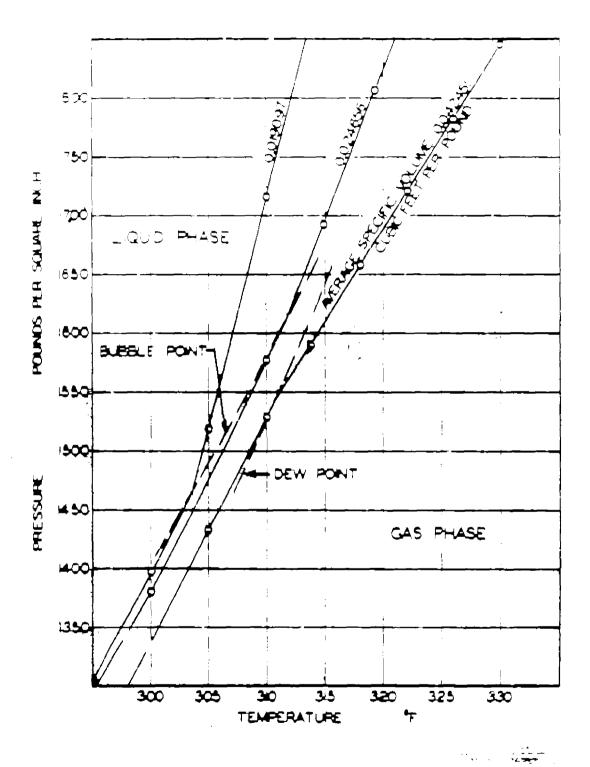


Fig. 3 Behavior of a Mixture Containing 0, 9431 Weight Fraction Nitrogen Dioxide in the Heterogeneous Region.

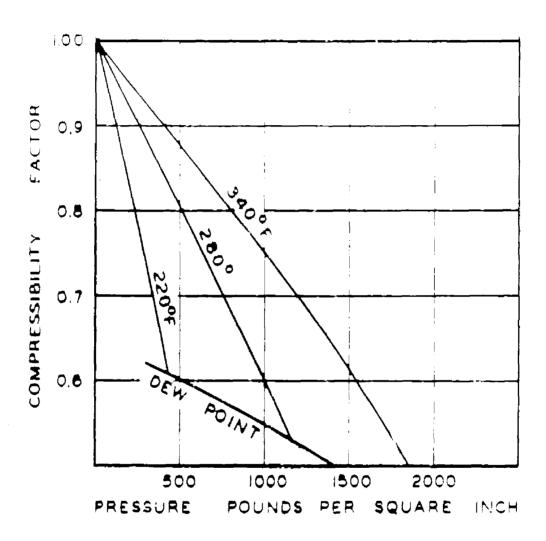


Fig. 4 Compressibility Factor for a Mixture Containing 0, 8312 Weight Fraction Nitrogen Dioxide.

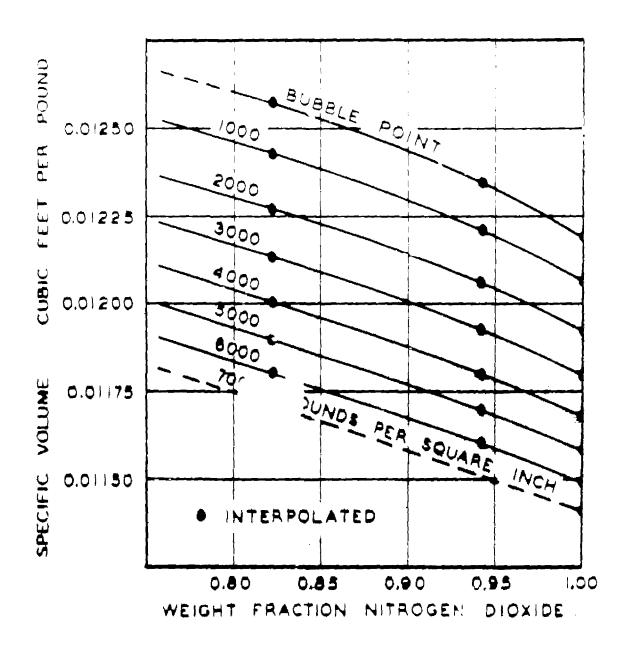


Fig. 5 Specific Volume-Composition Diagram for a Temperature of 160° F.

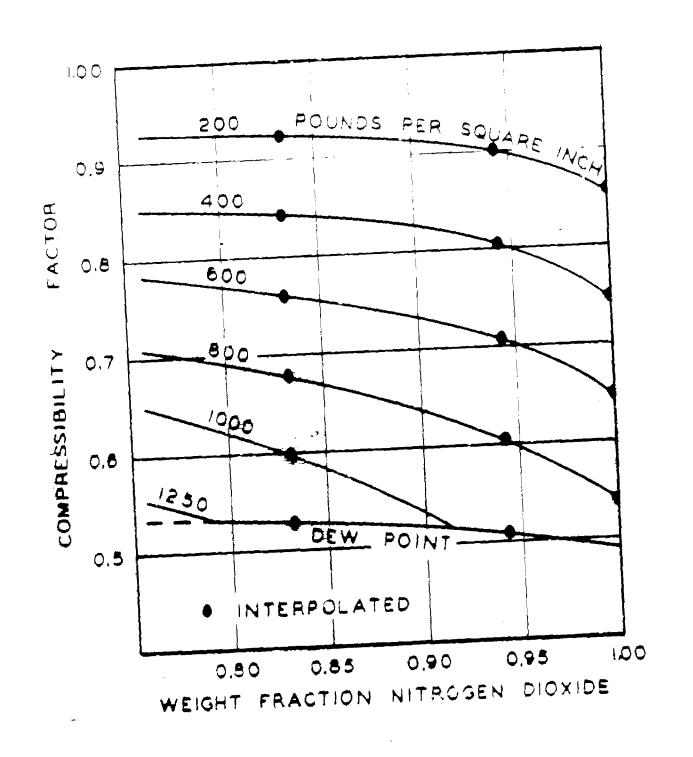


Fig. 6 Effect of Composition upon Compressibility Factor at 280° F.

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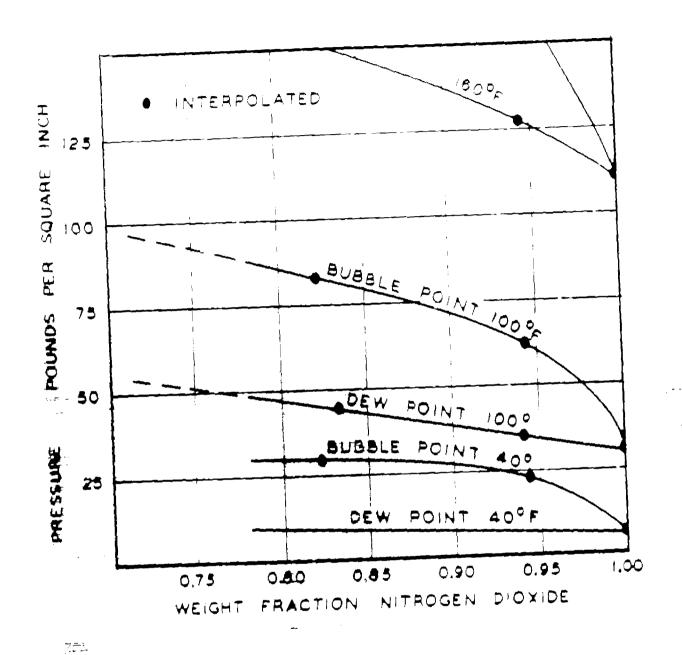


Fig. 7 Pressure-Composition Diagram for the Lower Temperatures.

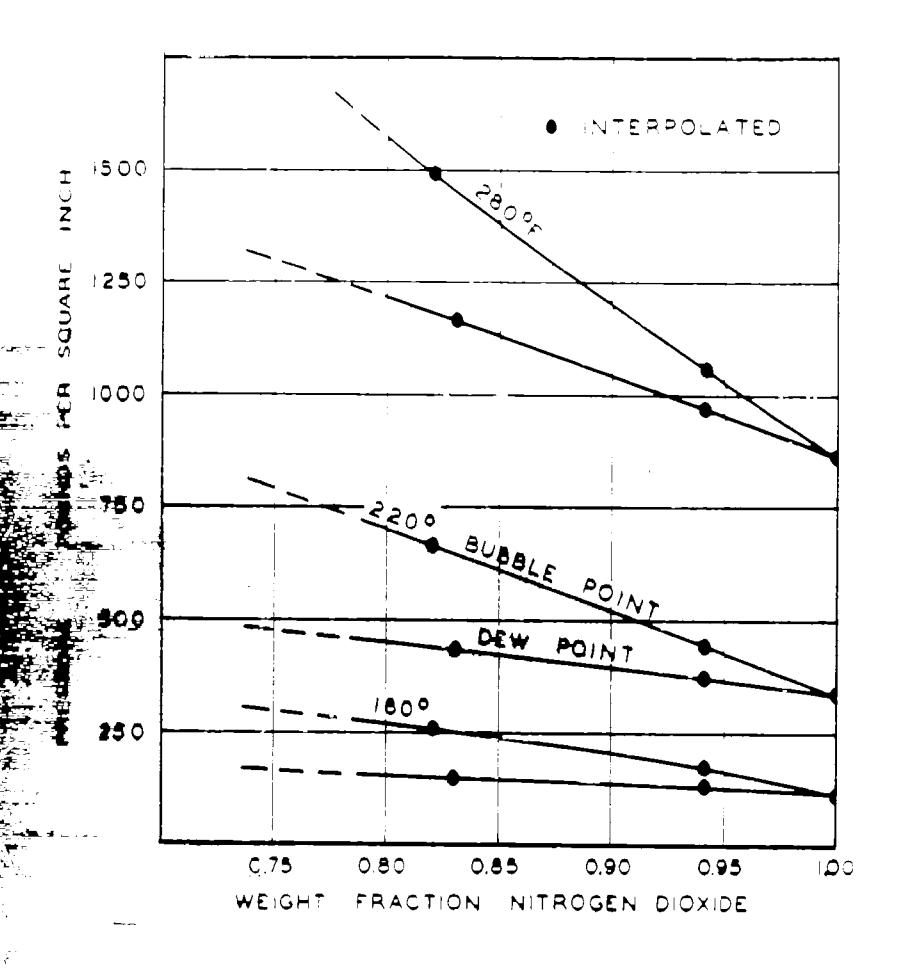


Fig. 8 Pressure-Composition Diagram for the Higher Temperatures.

## TABLES

- I. Sample of Experimental Results
- II. Volumetric Behavior of Mixtures of the Nitric Oxide-Nitrogen Dioxide System
- III. Properties of the Coexisting Phases in the Nitric Oxide-Nitrogen Dioxide System.

TABLE I

# SAMPLE OF EXPERIMENTAL RESULTS

# Weight Fraction Nitrogen Dioxide= 0, 94305

## TABLE II

THE CONTROL OF THE STATE OF THE

# VOLUNETRIC BEHAVIOR OF MIXTURES OF THE NITRIC CXIDE-NITROGEN DIOXIDE SYSTEM

Weight Fraction Nitrogen Dioxides 0, 95

Fressure, Lb. /Sq. Inch Absolute	Specific Volume, Cu. Ft. /L5.	Compressi- Mility Factor	Specific Volume, Cu. Ft. /Lb.	Compressi- bility Factor	Specific Volume, Cu. Ft./Lb.	Compr <b>e</b> ssi- bility Ector
	40	40°F.	160	100°F.		160°F.
Dew point	-	- B(CC)	-	;	١	; ,
Rubble point	7) q£6010°0	0700'0	0.011559	0.0052	0.012326	(102) 0, 0135
200	0.01092	0. 6182	0.011541	0.0172	0.012319	9.0166
400	0.01090	0.0364	0.011519	0.0344	0.012288	0.0331
009	0.01089	0.0546	0.011496	0.0515	0.012256	6.0496
800	0.01088	0.0727	0.011474	0.0635	0.012224	6,0659
1000	0.01086	0.0907	0.011453	0.0854	0.012190	0.0521
1250	0.01084	0.1132	0.011429	9901.0	0.012152	0.1624
1500	0.01083	0.1357	0.011402	0.1275	0.012118	0. 1225
1750	0.01081	0.1581	0.011381	0. 1486	0, 012081	0.1425
2000	0.01079	û. 1803	0.011359	0. 1695	0. 012048	0 1624
2250	0.01078	0.2027	0.011338	0. 1903	0.012013	0.1821
2500	0.01076	0.2248	9.611316	0.2111	0.011980	0.2018
2750	0.01074	0.2468	0.011292	0.2317	0.011946	0.2214

Figures in parentheres represent dew point or bubble point pressures expressed in lb. /sq. inch. Specific volumes for 40° F. are extrapolated. a

Specific volumes at 7000 lb. /sq. inch for all temperatures are extrapolated.

TABLE II (cont.)

## Weight Fraction Nitrogen Dioxide= 0, 95

Pressure, Lb. /Sq. Inch Absolute	Specific Volume,	Compressi- billity Factor	Specific Volume,	Compressi-billty Factor	Specific	Compressiv
	200. Ft. / L.B. 220°F.	Ĭr.	٥	2800E	ą	othty zactor
Dew point	0. 2697 <sup>d</sup> (364)	0.6034	(953)	3) 6 5070	34	340°F.
Bubble point	(424) 0. 013504	0. 0352	(1026) 0. 016064	_		
200	0, 6404	0. 7869	0. 7945	0.8970	25#96 O	3
009	0.013444	0.0496	0.3538	0. 7989	0.4299	0, 9488 0, 8979
008	0.013380	0.0658	0. 1324	0.5979	0. 2704 0. 1916	0.8473
1000	0.013320	0.0818	,		•	0061.3
le su	0.013249	0.1017	0.015730	, .	0. 1432	0.7476
1500	C. 013181	0. 1215	0.015424	0.1111	0, 1043	V. 6653
1750	0.013117	0. I-110	0.015165	0. 1498	0.07743	0, 6065
2000	0.013651				20100	٥. 5215
2250	0.012990	0. 1504	0.014944	0. 1687	0. 03890	0.4962
2500	0.012929	0.1790	0.014765	0.1875		7
2750	0.012869	0.2174	0.014607 0.014466	0. 2062 0. 2246		
3000	0.012811	1310				
3500	0.012707	0.2331	0.014339	0.2428		
4.000	0.012609	0 3000	0.014115	0.2789		
4500	0,012523	0.3462	0.013918 0.013740	0.3143 0.3490		
2000	0, 012442					
0009	0.012788	0.3822	0.013588	0.3835		
7000	0.012339°	0. 5220	0.613318 0.013000C	0.4511		
Lew point volume	n are estimated,	d,	0/0710:0	3, 5163		
voluntes 101 3	volumes for 340° F. are extrapolated.	olated.				

TABLE II (cont. )

# Weight Fraction Mitrogen Dioxide = 0.90

Compressi- bility Factor	ióu^k.	(264)	0.010.0		0.0163	0.0328	0.0487		0.0807	0 1006	0.1263	0, 1400		0.1595	0.1789	0.1982	0.2174		0. 2364	0.2514	0.3119	0.3493	i	0.3865	0.4600	0, 5323
Specific Volume, Gu. Ft. /Lb.		· (2)	0.612431	0.015431	0.013364	0.012390	0.012328		0.012253	6. 012252	0.012233	0.012178	,	0.012141	0.012104	0.012069	0.012035	90000	0.0170.0	0. UI 1938	0.011872	c. 011819	9000	0.01170	0.011674	0.011579 <sup>c</sup>
Compressi- billity Factor	100°F.		0.0060	910 0	0.0338	0.0505	0.0672		0.0839	0. 1046	0. 1253	0.1459		U. 1664	0. 1868	0.2072	0.2274	0 2476	7 2070	0,07.0	0. 3275	0.3671	0 4066	0.4040	D. 4846	0.5614
Specific Volume, Cu. Ft./Lb.	01	(71)	0.011648	0.011631	0.011608	0, 011582	0.011561	•	0.011539	0.011511	0.011488	0.011463		0.011441	0.011418	0.011397	0.011372	0.011350	0 011307	0.0110	0.011239	0.011218	0.011182	701110.0	0.011105	0.011029
Compressi- bility Factor	40°F.		0.0024	0.01780	0.0358	0.0537	0. 9715			0.1114	0.1334	0.1554	0 1774	0 1007	0.1772	0.2209	0. 2426	0.2642	0.3073	0 3502	2000	0.3929	0.4350	0 5185	6.010.0	0.6015
Specific Volume, Cu. Ft./Lb.	40,	(27)	0. 01103	0.01102	0.01100	0.01099	6.01097		0. 01095 0. 0105	0.01094	0.01092	0.01090	0.01089	0.01087	0.01086	6,010,0	v. 01083	0.01081	0.01078	0, 01075		0.91016	0.01068	0.01061	322010	0.01055
Pressure, Lb. /Sq. Inch Absolute	Dew point	Darkette	nuod algana	700	400	009	800	1000	996	0071	0061	1430	2000	2250	2500	2750	2	3000	3500	4000	4500		9009	6000	7000	2005

TABLE II (cont.)

Weight Fraction Nitrogen Dioxide: 0, 90

Pressure, Lb. /Sq. Inch Absolute	Spectfic Volume, Cu. Ft./Lb.	Compressibility Factor 220°F.	Specific Volume, Cu. Ft. /Lb.	Compressibility Factor 280°F.	Specific Volume, Cu. Ft./Lb.	Gompressi bility Factor 340 <sup>0</sup> F.
Dew point	(3) 0, 2592 <sup>d</sup>	(394) 0.6110 (516)	0.09042 <sup>d</sup>	(1043) 0.5188		
Bubble point	0.013640	0.0421	0.016283	0.11132		
007	0.6784	0.8125	0.8303	0.9137	0. 9373 <sup>©</sup>	0.9541
400	1		0.3760	0.8275	0.4460	0.9079
600	0.013668	0.0489	0.2221	0, 7334	0.2822	6198-0
800	0.013533	0.0648	0.1449	0.6379	0.2007	0.8172
1000	0.013467	0. 0806	0.09805	0.5395	0. 1515	0.7711
1250	0.013387	0.1002	0.016209	0.1115	0.1119	0.7126
1500	0.013317	0.1196	0.015851	0.1308	0.08446	0.6448
1750	0.013249	6, 1388	0.015525	6.1495	0.06413	9, 5712
2000	0.013182	0.1579	0.015257	0.1679	0.04724	0.4809
5250	0.013119	0.1768	0.015036	0.01862		
2500	0.013059	0. 1955	0.014848	0.2042		
2750	0.013000	0.2141	0.014687	0.2222		
3000	0.012944	0.2325	0.014542	0.2400		
3500	0.012938	2690	0.014310	0.2756		
4000	0.012739	3.3051	0.014106	6.3105		
4500	0.012650	0.3409	0.013921	0,3447		
5000	0.012568	0.3763	0.013758	0.3785		
6000	0.012408	0.4458	0.013478	0.4450		
2000	0.012257 <sup>c</sup>	0, 5138	0.013231 <sup>c</sup>	9605.0		

TABLE II (Cont.)

Weight Fraction Nitrogen Diaxide= 0,85

Pressure, Lb. /Sq. Inch Absolute	Specific Volume, Cu. Ft. / Lb.	Compressi- bility Factor	Specific Volume, Cu. Ft. /Lb.	Compressi- ballity Factor	Specific Volume, Gu, Ft. /I.b.	Compressi- billity Factor
Dew point	<b>0</b>	40°F.	9;	100 <sup>0</sup> F.		160°F.
•	(62)		(79)	- 6	( <del>)</del>	- (6)
Bubble point	0.01113	0. 6026	0.011736	9900 0	0.012527	0.0192
007	0.01112	0.0177	0.011723	0.0366	ı	;
400	0.01110	0.0353	0.011700	0.0332	0.012491	0.0320
009	0.01109	0.0528	0.011669	0.0496	0.012455	0.0359
800	0.01107	0.0704	0.011643	0.0660	0.012419	0.0636
1000	0.01105	0,0878	0.011619	0.0824	. 185210 0	0.0703
1250	0.01103	0.1095	0.011590	0, 1027	0.012346	8860 O
0061	0.01103	0.1312	0.011562	0, 1230	0.012299	0 1182
1750	0. 61699	0.1528	0.011539	0, 1432	0.012262	0.1374
2006	0.01097	0.1743	0.011511	0, 1633	0.012228	9951 0
2250	0.01095	0, 1957	0.011489	0, 1833	0.012190	0.1757
2500		0.2171	0.011466	0. 2033	0,012357	0.1947
2750	0. 01 <b>091</b>	0, 2393	0.011441	0.2231	0.012121	0.2135
3060	0.01089	0,2595	0.011419	0.2430	0, 612089	6.25.2
3500	0.01086	0.3020	0.011376	0.2824	0.012026	0.2696
4000	0.01082	0, 3438	0.011329	0.3214	0.011961	0,3065
4500	0.01079	0,3857	0.011289	0.3603	0.011905	0.3432
2000	0.01075	0.4270	0.011251	05 <b>68</b> .0	0.011853	3336
0009	0.01063	0.5096	0.011175	0.4755	652110 9	0.53.4 G
2000	0.01061	0.5900	0.011100 <sup>C</sup>	0.5511	0.011664	0.5236

TABLE II (cont. )

# Weight Fraction Nitrogen Dioxide = 6, 85

Compressi- bility Factor 5. 340°F.			0.9581 6.9156	0. 8731 0. 8309	0 7887	0. 7331	0.6737 6.6096		1 525 0									
Specific Volume, Gu. Ft./Lb. 340			0.9651° 0.4611	0, 2932 0, 2092	0.1588	0.1182	0. 09048 0. 07018	000.00	6, 03CU									
Compressibility Factor 260°F.	(1132) 0. 5268	(1388) 0. 1237	0.9219	0.7547 0.6700	0.5841	, ,	0.1589	0 1672	0. 1848	0.2025	0.2201	7286 11	0.52.0	0. 3070	0.3409	0 3743	0.4392	0.5030
Specific Volume, Cu. Ft./Lb.	0.08671 <sup>d</sup>	0.016611	0.8589	0. 2344 0. 1561	0.1088	- 0 016341	0.016916	0.015579	0.015309	0.015094	0.014914	0.014761	0.014511	0.014300	0.014118	0.013948	0.013641	0.013389 <sup>c</sup>
Compressibility Factor	0.6087	0.0490	0, 8209 0, 6320	0.0639	0.0795	0, 0987 0, 1178	0. 1388	0.1555	0.1741	0.1926	0.2109	0.2290	0.2650	0.3006	0.3358	0.3705	0.4390	0.5060
Specific Co Volume, bill Cu. Ft./Lb.	0.2471 <sup>d</sup> (422)	0.013765	0, 7028 0, 2705	6, 013685	0.013609	0.013449	0.013579	0.013311	0.013251	0.013189	0.013130	0.013072	0.012967	0.012869	0.012778			$0.012378^{C}$
Fressure, Lb. /Sq. Inch Absolute	Dew point	Bubble point	700 400 909	800	1000	1500	1750	2000	0577	0062	0013	3000	3500	4500	006	2000	0000	0007

TABLE II (cost.)

# Weight Fraction Mitrogen Dioxide = 0.80

Pressure, Lb. /Sq. Inch Absolute	Specific Volume, Cu. Ft./Lb.	Compression billity Factor 40°F.	Specific Volume, Cu. Ft. /Lb.	Compressi-bility Factor	Specific Volume, Cu. Ft./Lb.	Compressibility Factor 160° F.
Dew point		, ·		- (98)	- (2	(270)
Bubble point	0.01125b	0. 9026	0.011828	0.0070	0.012606	0, 04.15
200	0.01123	0.01741	0.611810	0. 6163	i	,
400	0.01120		0.011781	0.0326	6.012578	0.0314
009	0,01118	0.0520	0.011758	0.0488	9.012538	0.6470
800	0.01116	0.0692	0.011730	0.0650	0.012499	9790.0
3000	0.01115	980.0	0, 011757	0.0810	0.012461	0.0779
1250	0.01112	0.1078	0.011576	0.1010	0.012419	0.6970
1500	0.01110	0.1291	c. 011649	0. 1269	0.012378	0, 1161
1750	0.01108	0, 1503	0.011620	0, 1407	0.012339	0.1350
7000	0, 01106	0, 1715	0.011590	0, 1604	0.012302	0, 1538
2250	0.01104	0.1926	0.611566	0.180)	6.012268	0.1726
2500	0.01102	0.2136	0.011539	0.1997	0.012232	0. 1912
2750	0.01100	0.2345	0.011512	0.2191	0.012199	0.2097
3000	0.01098	0.2554	0.011489	0. 2386	0.012168	0, 2282
3500	0.01095	0.2971	0.011438	0.2771	0.012104	0.2648
4000	0.01091	6, 3383	0.011391	0.3154	0.012041	0.3011
4500	0.01087	0.3792	0.011358	0.3538	0.011988	0.3372
5000	0,01083	0.4198	0.011320	0.3917	0.011939	0.3732
0009	0.01076	0.5005	0.011246	0.4670	0.611839	C. 4441
7000	0.01068	0.5796	0, 011170 <sup>c</sup>	0.5412	0.011742 <sup>C</sup>	0.5138

TABLE II (cont.)

Weight Fraction Bitragen Bloxides 0,80

Pressure, Lb. /Sq. Inch Absolute	Specific Cor Volume, bill Cu. Ft. /Lb. 220°F.	Compressibility Factor F.	Specific Volume, Cu. Ft. / Lb.	Compressi- bility Factor 280°F.	Specific Volume, t Cu. Ft. /Lb. 340 <sup>o</sup> F	Compressi- bility Factor
Dew point	0.2340 <sup>d</sup> (701)			(1217) 0, 5315 (1570)		
turod arggner	0.013071	4000 O	6. 01 /0/5	0, 1404		
200	0. 7223	0.8234	0.8940	0.9259	0.9917	0.9668
400	0.2841	0.6476	0.4043	0.8469	0.4753	<b>δυ</b> ζ <b>ό υ</b>
009	•	1	0.2451	0. 7762	0.3031	0.8810
800	0.013830	0.0631	0. 1656	0.6939	0.2169	0.8406
1000	0.013749	0.0784	0. 1183	8619.0	0, 1653	£.8008
1250	0.013658	0.0973	4	٠	0, 1237	0.7492
1500	0.013574	0.1160	•	ı	0.09576	0.6958
1750	0.013500	0.1346	0.016391	0. 1502	6, 07525	0.6375
2000	0.013431	0. 1531	0.015938	0. 1669	0.06054	0.5865
2250	0, 013371	0.1715	0.015601	0. 1838		
2500	0.013312	0. 1897	0.015350	0. 2010		
2750	0.013253	0.2077	0.015150	0, 2182		
3000	0.013199	0.2257	0.014989	0.2355		
3500	0.013089	0.2611	0.014721	0.2698		
4000	0.012990	0.2962	0.014509	6, 3039		
4500	0.012900	0.3309	0.014318	0.3374		
2000	0.012816	0.3652	0.014146	0.3704		
0009	0.012651	0.4326	0.013831	0.4346		
7000	0.012498c	0.4936	0.013566	0.4971		

TABLE II (cont.)

Weight Fraction Nitrogen Dioxide - 0, 75

Pressure, Lb. /Sq. Inch Absolute	Specific Volume, Cu. Ft. / Lb.	Compressibility Factor billty Factor	Specific Volume, Cu. Ft. /Lb.	Compressibility Factor 100°F.	Specific Volume. Gu. Ft./Lb.	Compressibility Eactor
Dew point	(30)	1	- (63)	1	ı	(887)
Bubble point	0.01134b	0. 6026	0.011923	0.0075	0.012679	0.6223
200	0.01132	0.0171	0.611902	0.0161	ı	1
00*	0.01130	0.0342	0.011873	0.0321	0.012651	0.0309
009	0.01128	0.0512	0.011847	0.0480	0.012609	0.0462
840	0.01125	0.0682	0.011819	0.0639	0.012571	0.0614
1000	6,01124	0.0851	0.011791	0.6797	5, 012532	0.0765
1250	0.01122	0.1062	6.011759	0.0993	9.012490	0.0954
1500	0.01119	0.1271	0.011728	0.1189	6,012450	c. 1140
1750	0.01117	0.1480	0.011698	0.1384	0.912412	0.1326
2000	0.01114	0. 1687	0.011669	0. 1577	0.012379	0. 1511
2250	0.01112	c. 1894	0.011640	0.1770	0.012345	0, 1696
2500	0.01110	0.2101	0.011611	0.1962	0.012313	0.1879
2750	0.01107	0.2304	0.011582	0.2153	0.012280	0. 2061
3600	0,01106	0.2512	0.011558	0.2343	0.012248	0.2243
3500	0.01162	0.2920	0.611510	0.2723	0.012181	0. 2662
4000	0.01098	0.3325	0.011461	0.3098	0.012119	0.2959
4500	0.01094	0.3727	0.011424	0.3474	0.012062	0.3313
5000	0.01094	0.4141	0.011389	0.3844	0.012011	9998.0
0009	0.01082	0.4914	0.011312	0.4587	0.011918	
7000	0.01074 <sup>C</sup>	0.5691	6. 011232 <b>c</b>	0.5314	0.011827 C	0.5054
•						

f All values of volume for this composition are extrapolated.

## TABLE II (cont)

## Weight Fraction Mitrogen Dioxide- 0.75

Pressure, Lb. /Sq. Inch Absolute	Specific Volume, Cu. Ft./11b.	Compressibility Factor 270°F.	Specific Volume, Cu. Ft. /Lb.	Compressi-bility Factor (280°F.	Specific C Volume, b Cu. Ft./Lb. 340°F.	Compressibility Factor <sup>2</sup> F.
Dew point Bubble point	0, 2199 <sup>d</sup> 0, 013980	(475) 0.5813 (790) 0.0615	(1312) 0.0795 <sup>d</sup> (16 <del>4</del> 3) 0.017619	12) 0, 5335 43) 0, 1480		
200	7411	0.8249	0.9072	0.9279	1.017 0.4884	0.9619
009 800	0.013978	0.9579	0. 2546 0. 1741	0. 7812 0. 7125	0. 3122 0. 2241	0.5861 0.8480
1000	0.013889	0.0773	0. 1263 0. 0875	0.6459	0.1712	6, 8099 0, 7625
1500	0.013705 0.013626	0. 1144 0. 1327	0.017058	0.1527	0. 1005 0. 07975	6. 7129 6. 6606
2000 2250 2500 2750	0. 013551 0. 013491 0. 013431 0. 013372	0.1508 0.1689 0.1869 0.2046	0.016401 0.015949 0.015629 0.015401	0, 1678 0, 1835 0, 1998 0, 2166	0. 66418	0.6072
3000 3500 4000 4500	0. 013319 0. 013215 0. 013116 0. 013029	0, 2224 0, 2574 0, 2920 0, 3263	0.015224 0.014941 0.014713 0.014521	0. 2336 0. 2674 0. 3010 0. 3342		
50 <b>00</b> 60 <b>00</b> 70 <b>00</b>	0. 012943 0. 012781 6. 012619	0.3602 0.4268 0.4916	6. 014346 6. 014022 0. 013732	0.3668 0.4302 0.4916		

PROPERTIES OF THE COFXISTING PHASES IN THE NITRIC OXIDE-NITROGEN DICKIDE SYSTEM

TABLE III

Pressure, Lb. Şq. Inch	Weight Nitroge		Specific Cu. Ft	Volume, ./Lb.
Absolute	Dew Point	Bubble Point	Dew Point	Bubble Point
		⊕c <sup>o</sup> ₽.		
6.5ª	1.0000	1.006 <b>0</b>	), 158	0.01034
8.C	C.8 <b>74</b> 5	0.995 <b>6</b>	•	0.01034
9. C	0.8015	0.9931	-	0.01034
10. C	0.762	<b>0</b> .990 <b>7</b>	<b>4</b> .	0.01035
<b>15.</b> C	-	0.9 <b>770</b>	-	0.01038
20.C	•	0.9588	•	0.01041
25.0	•	0.927 <b>4</b>	-	0.01047
		100°F,		•
30. 7 <sup>a</sup>	1.0000	1,000 <b>0</b>	2.5190	9. 011439
3 <b>5.</b> C	0.9454	0, 9958		0.011449
40.0	0.8845	0.9901	Tage 1	0.011461
<b>45.</b> 0	0.8272	0.9832	•	0.011479
50.0	0.7706	0.9750	•	0.011500
60. C	•	0.9504	_	0.011557
70.0	•	0.907 <b>3</b>	-	0.011635
80.0		0.8421	L	0.011750
90.0	•	0.7701	•	0.011881
		160°F.		
111. 2 <sup>a</sup>	1.0000	1.0000	6.773 <b>3</b>	0.012188
120.0	0.9701	0.9920		0.012211
130.0	0.9329	0.9824	•	0.012239
140.0	0.8870	0.9729	_	0.013264
150.0	0.8311	0.9625	•	0.012290
175.0	•	0.9354	_	0.012336
200.0	•	0.9052	~	0.012422
225.0	•	0.8714	_	0.012488
250.0	•	0.8331	•	0. 012553
27 <b>5</b> . 0	<b>→</b>	C.7867	•	0.012622

a Vapor pressure of mitrogen dioxide

b Dew point volumes are estimated

## TABLE IN(cont.)

Pressure	Weight Fraction Nitrogen Dioxide		Specific Volume,  Gu. Pt. 'Lb.	
Lb./Sq. Inch				
Absolute	Dew Point	Bubble Foint	Dew Point	Bubble Point
		220°F.		
332. 8ª	1,0000	1.0000	0.2743	0.013343
<b>3</b> 50. (	C.9728	0.9899	0.2733 <sup>b</sup>	0.013373
375. C	0.9319	0.9767	0.2654	0.013418
400.0	0.888 <b>7</b>	0.9631	0.1566	0.013460
<b>4</b> 25. C	0.8438	0.9498	0.2457	0.01 <b>35</b> 05
450.0	0.7978	0.9361	0, 2 <b>334</b>	0.013544
<b>500</b> . c	-	0.9091	<b>6</b> ~	<b>0.</b> 01 <b>3</b> 619
600. r		0.8549	L-	0.013751
700.0	•	o.8 <b>003</b>	**	O.013870
		280°F.		
864. 1 <sup>a</sup>	1.0000	1,0000	0.0984	0.015924
900.0	0.9797	0.9884	0.0968 <sup>b</sup>	0.015949
950.0	0.9518	0.9730	0.0943	0.015990
1000.0	0.9240	0.9575	0.0905	0.016037
1050.0	0.8959	0.9428	0.0900	0.016092
1100.C	0.8678	0.9282	0,0888	0.016149
1200.0	0.8103	0.9002	0.4840	0.016282
1300.0	-	0.8733	*	0.016447
1400.0	-	0.8467	•	0.016639
1500.0	-	0.3 <b>29</b> 8	•	0.016780